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Light-shining-through-wall cavity setups for probing ALPs

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Introduction

- Axions and axion-like particles (ALPs) are hypothetical pseudoscalar particles. They are massive and electrically neutral.
- Axion as CP-strong problem solution [Peccei-Quinn, 1977].
- Axions and ALPs as a part of dark matter content [Preskill, Abbott, Dine, 1982].
- Interaction with EM-field is described by the following term of the Lagrangian and the corresponding vertex:

The mass of m_a and the coupling constant of $g_{a\gamma\gamma}$ are related for QCD axion as follows, $g_{a\gamma\gamma} = 10^{-10} \,\text{GeV}^{-1}\left(\frac{m_a}{1 \,\text{eV}}\right)$. These parameters are independent for ALPs.

Detection methods



Figure 1 – The experiments for axions and ALPs search. a) haloscope, b) LSW, c) helioscope (CAST).

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Current limitations



Figure 2 – The current limitations on parameters $(m_a, g_{a\gamma\gamma})$ for QCD axions and ALPs.

LSW experimental setups



FIG. 7: Photo of emitting cavity (1) and shielding enclosure (2) containing the identical detecting cavity. For ALP search, both parts were placed in the bore of a solenoid magnet with the same arrangement as shown in the picture.



FIG. 1. Left: The experimental setup for the Dark SRF experiment consisting of two 1.3 GHz cavities. Right: A sketch of the Dark SRF electronic system.

Figure 3 – The experimental setups photos. The left panel presents the CROWS experiment at CERN [Betz *et al.*, 2013]. The right panel presents the current Fermilab experimental setup [Romanenko *et al.*, 2023]. Results were published for Dark photons search only. The SRF experimental setup at CERN is projecting [Bogorad *et al.*, 2023].

Motivation and aims

- The LSW cavity setups are being developed at the moment
- The problem of their sensitivity improvement is important
- The research aims were
 - comparison of various cavity types (normal conducting and superconducting RF) schemes of the LSW cavity setups
 - finding the optimal geometrical configuration
 - discussion of schemes technical features

Experimental model scheme



Figure 4 – The experimental model schemes for two cavity orientations: coaxial (the left panel) and parallel (the right panel).

Cavity type	B_0	$B_{\rm ext}$	Q	P
Normal conducting RF	$0.01\mathrm{T}$	$3\mathrm{T}$	10^{5}	$100\mathrm{kW}$
Superconducting RF	$0.1\mathrm{T}$	-	10^{10}	$0.1\mathrm{kW}$

Table 1 – The basic characteristics of normally conducting RF and SRF cavities. Four setups were considered:

7/16 i) RF+RF, ii) SRF+SRF, iii) SRF+RF, iv) RF+SRF.



Theory

• The motion equations

$$\left(\partial_{\mu}\partial^{\mu} + m_{a}^{2}\right)a = -\frac{g_{a\gamma\gamma}}{4}F_{\mu\nu}\tilde{F}^{\mu\nu},\tag{1}$$

$$\partial_{\mu}F^{\mu\nu} = -g_{a\gamma\gamma}\,\tilde{F}^{\mu\nu}\partial_{\mu}a = j^{\nu}_{a}.\tag{2}$$

■ In the electric and magnetic field terms it reads

$$\left(\partial_{\mu}\partial^{\mu} + m_{a}^{2}\right)a = g_{a\gamma\gamma}\left(\vec{E}\cdot\vec{B}\right),\qquad(3)$$

$$(\vec{\nabla} \cdot \vec{E}) = \rho_a, \quad [\vec{\nabla} \times \vec{B}] = \frac{\partial \vec{E}}{\partial t} + \vec{j}_a,$$
 (4)

where

$$\rho_a = -g_{a\gamma\gamma}(\vec{\nabla}a \cdot \vec{B}) , \quad \vec{j}_a = g_{a\gamma\gamma}([\vec{\nabla}a \times \vec{E}] + \dot{a}\vec{B}) .$$
 (5)

Generated signal

■ The exact Klein-Gordon equation solution is

$$a(t,\vec{x}) = g_{a\gamma\gamma} E_0^{\rm em} B_0^{\rm em} \operatorname{Re} \left[\int_{V_{\rm em}} d^3x' \left(\vec{\mathcal{E}} \cdot \vec{\mathcal{B}}\right)(\vec{x}') \frac{e^{ik_a |\vec{x} - \vec{x}'| - i\omega_a t}}{4\pi |\vec{x} - \vec{x}'|} \right].$$
(6)

The exact Maxwell's equations solution is

$$\vec{E}(t,\vec{x}) \simeq \operatorname{Re}[G\vec{\mathcal{E}}_s(\vec{x})e^{-i\omega_s t}], \quad \vec{B}(t,\vec{x}) \simeq \operatorname{Re}[G\vec{\mathcal{B}}_s(\vec{x})e^{-i\omega_s t}], \quad (7)$$

$$G = -\frac{Q_{\rm rec}}{\omega_s} \cdot \frac{1}{V_{\rm rec}} \int\limits_{V_{\rm rec}} d^3x \, (\vec{\mathcal{E}}_s^* \cdot \vec{j}_a) = i Q_{\rm rec} g_{a\gamma\gamma}^2 E_0^{\rm em} B_0^{\rm em} B_0^{\rm rec} V_{\rm em} V_{\rm rec} \mathcal{G} \delta^{-1}, \tag{8}$$

$$\mathcal{G} = \int_{V_{\text{rec}}} \frac{d^3 x}{V_{\text{rec}}} \int_{V_{\text{em}}} \frac{d^3 x'}{V_{\text{em}}} \left(\vec{\mathcal{E}} \cdot \vec{\mathcal{B}}\right)^* (\vec{x}) \left(\vec{\mathcal{E}} \cdot \vec{\mathcal{B}}\right) (\vec{x}') \frac{e^{ik_a |\vec{x} - \vec{x}'|}}{4\pi} \frac{\delta}{|\vec{x} - \vec{x}'|} .$$
(9)

• For both cases of $\omega_a = \omega_0$ and $\omega_a = \omega_1 + \omega_2$ EM-invariant reads

$$(\vec{\mathcal{E}} \cdot \vec{\mathcal{B}}) = (\vec{\mathcal{E}}_0 \cdot \vec{\mathcal{B}}_{ext}), \quad (\vec{\mathcal{E}} \cdot \vec{\mathcal{B}})_+ = \frac{1}{2} (\vec{\mathcal{E}}_1 \cdot \vec{\mathcal{B}}_2 + \vec{\mathcal{E}}_2 \cdot \vec{\mathcal{B}}_1).$$
(10)

Experiment sensitivity

The signal power

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$$P_{\text{signal}} = \frac{\omega_s}{Q_{\text{rec}}} \int\limits_{V_{\text{rec}}} d^3x \, \langle |\vec{E}^2(\vec{x},t)| \rangle_t = \frac{\omega_s}{Q_{\text{rec}}} \cdot \frac{1}{2} |G|^2 V_{\text{rec}} \,, \qquad (11)$$

■ The radiometric equation

$$SNR = \frac{P_{\text{signal}}}{P_{\text{noise}}} \cdot \sqrt{t\Delta\nu} , \qquad (12)$$

where $P_{\text{noise}} = T\Delta\nu$ – the thermal noise power ($\omega_s \ll T$). The sensitivity estimation

$$g_{a\gamma\gamma} = \left[\frac{2\delta^2 T \,\text{SNR}}{\omega_s Q_{\text{rec}} E_{0,\text{em}}^2 B_{0,\text{em}}^2 B_{0,\text{rec}}^2 V_{\text{em}}^2 V_{\text{rec}} |\mathcal{G}|^2}\right]^{\frac{1}{4}} \left(\frac{\Delta\nu}{t}\right)^{\frac{1}{8}}, \quad (13)$$

where $\Delta\nu = \frac{\nu_s}{Q_{\text{rec}}} \text{ or } \Delta\nu = \frac{1}{t} \text{ [Bogorad, 2019]}$

RF + RF scheme sensitivity



Figure 5 – The sensitivity dependence $g_{a\gamma\gamma}$ for the RF+RF scheme on the R/L ratio for the cases of $m_a = \omega_a$ and $m_a = 0$ (the left panel) and on the mass in the case of an optimal value of the R/L ratio (the right panel). The coaxial and parallel orientations are considered. The cavities volume is $V = 1 \text{ m}^3$, the distance between cavities walls $\delta = 0.5 \text{ m}$, the EM-mode is TM_{010} , the experiment duration is $t = 10^6 \text{ s}$.

SRF + SRF scheme sensitivity



Figure 6 – The sensitivity dependence $g_{a\gamma\gamma}$ for the SRF+SRF scheme on the R/L ratio for the cases of $m_a = \omega_a$ and $m_a = 0$ (the left panel) and on the mass in the case of an optimal value of the R/L ratio (the right panel). The coaxial and parallel orientations are considered. The cavities volume is $V = 1 \text{ m}^3$, the distance between cavities walls $\delta = 0.5 \text{ m}$, the EM-modes are $\text{TM}_{010} + \text{TE}_{011}$, the experiment duration is $t = 10^6 \text{ s}$.

SRF + RF scheme sensitivity



Figure 7 – The sensitivity dependence $g_{a\gamma\gamma}$ for the SRF+RF scheme on the R/L ratio for the cases of $m_a = \omega_a$ and $m_a = 0$ (the left panel) and on the mass in the case of an optimal value of the R/L ratio (the right panel). The coaxial and parallel orientations are considered. The emitter volume is $V = 1 \text{ m}^3$, the distance between cavities walls $\delta = 0.5 \text{ m}$, the emitter pump EM-modes are TM₀₁₀+TE₀₁₁, the signal receiver mode is TM₀₁₀, the experiment duration is $t = 10^6 \text{ s}$.

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RF + SRF scheme sensitivity



Figure 8 – The sensitivity dependence $g_{a\gamma\gamma}$ for the RF+SRF scheme on the R/L ratio for the cases of $m_a = \omega_a$ and $m_a = 0$ (the left panel) and on the mass in the case of an optimal value of the R/L ratio (the right panel). The coaxial and parallel orientations are considered. The receiver volume is $V = 1 \text{ m}^3$, the distance between cavities walls $\delta = 0.5$ m, the pump emitter EM-mode is TM₀₁₀, the receiver modes are TM₀₁₀+TE₀₁₁, the experiment duration is $t = 10^6$ s.

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Results and conclustions

Scheme type	$B_0^{\mathrm{em},(1)}$	$B_0^{\rm em,(2)}$	$B_0^{\rm rec}$	$Q_{\rm rec}$	$P_{\rm em}$	$ \mathcal{G} $	$g_{a\gamma\gamma}$
RF em. + RF rec.	$0.01\mathrm{T}$	3 T	$3 \mathrm{T}$	10^{5}	$100\mathrm{kW}$	10^{-2}	$3 \times 10^{-11} {\rm GeV^{-1}}$
SRF em. + SRF rec.	0.1 T	0.1 T	$0.1\mathrm{T}$	10^{10}	$0.1\mathrm{kW}$	10^{-3}	$5 \times 10^{-11} {\rm GeV^{-1}}$
SRF em. + RF rec.	0.1 T	0.1 T	3 T	10^{5}	$0.1\mathrm{kW}$	10^{-3}	$3 \times 10^{-10} \mathrm{GeV^{-1}}$
RF em. + SRF rec.	0.01 T	3 T	0.1 T	10^{10}	$100 \mathrm{kW}$	10^{-3}	$9 \times 10^{-11} \text{GeV}^{-1}$

Table 2 – The comparison of various schemes characteristics values. The geometric form-factor $|\mathcal{G}|$ and the experiment sensitivity $g_{a\gamma\gamma}$ are presented for the optimal R/L ratio for coaxial orientation and the low masses limit (area of $m_a \leq \omega_a/2$).

- Both RF+RF and SRF+SRF schemes allow to obtain similar values of the sensitivity at the level of $g_{a\gamma\gamma} \simeq (3-5) \times 10^{-11} \text{GeV}^{-1}$. Mixed schemes expectations are several orders weaker.
- The coaxial orientation with the ratio of $R/L \simeq 1.6$ is the most optimal geometrical configuration.
- The narrowest bandwidth of $\Delta \nu = 1/t$ is the important issue.

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• The disadvantage of RF+RF scheme is high emitter power, the disadvantage of SRF+SRF scheme is a more complicated signal photons detection against the pump mode background.

Thank you!



